AD-A078 928

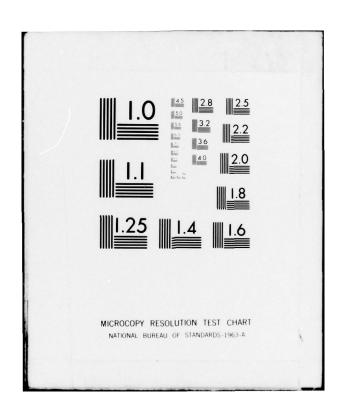
KIMBALL (L ROBERT) AND ASSOCIATES EBENSBURG PA
NATIONAL DAM INSPECTION PROGRAM. HUNTERS LAKE DAM (NDS ID NUMBER-ETC(U)
AUG 79 R J KIMBALL

DACW31-79-C-0009
NL

DACW31-79-C-0009
NL

END
AUG 10

END



00 AD A 0 7892

SUSQUEHANNA RIVER BASIN TROUT RUN, SULLIVAN COUNTY



PENNSYLVANIA

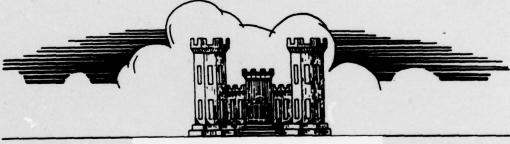
HUNTERS LAKE DAM

NDS ID NO. PA-356 **DER ID NO. 57-1**

PENNSYLVANIA FISH COMMISSION

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM





Distribution Unlimited Approved for Public Release Contract No. DACW31-79-C-0009

Prepared By

L. ROBERT KIMBALL & ASSOCIATES CONSULTING ENGINEERS & ARCHITECTS EBENSBURG, PENNSYLVANIA

15931 ORIGINAL CONTAINS COLOR PLATES: ALL DIC REPRODUCTIONS WILL BE IN BLACK AND WHIT

FOR

DEPARTMENT OF THE ARMY BALTIMORE DISTRICT CORPS OF ENGINEERS BALTIMORE, MARYLAND

21203

SUSQUEHANNA RIVER BASIN TROUT RUN, SULLIVAN COUNTY



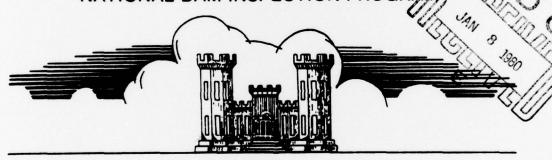
PENNSYLVANIA

HUNTERS LAKE DAM

NDS ID NO. PA-356 **DER ID NO. 57-1**

PENNSYLVANIA FISH COMMISSION

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRA



Prepared By

L. ROBERT KIMBALL & ASSOCIATES

CONSULTING ENGINEERS & ARCHITECTS EBENSBURG, PENNSYLVANIA

15931

FOR

DEPARTMENT OF THE ARMY BALTIMORE DISTRICT CORPS OF ENGINEERS BALTIMORE, MARYLAND 21203

AUGUST, 1979

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

PHASE I REPORT NATIONAL DAM INSPECTION REPORT

NAME OF DAM: Hunters Lake Dam STATE LOCATED: Pennsylvania COUNTY LOCATED: Sullivan

STREAM: Trout Run

DATE OF INSPECTION: May 24, 1979

ASSESSMENT

The assessment of the Hunters Lake Dam is based upon visual observations made at the time of inspection, review of available records and data, hydrology and hydraulic computations, and past operational performance.

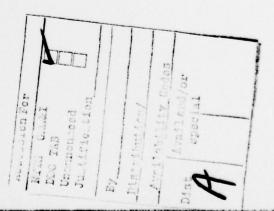
The inspection and review of data of Hunters Lake Dam did not reveal any problems which require emergency action. The dam appears to be stable, well maintained, safely operated and in good condition.

Hunters Lake Dam is a high hazard-intermediate size structure. The spillway design flood i the PMF.

The existing spillway and reservoir are capable of controlling the PMF (Probable Maximum Flood). Based on criteria established by the Corps of Engineers, the spillway is termed adequate.

The following recommendations and remedial measures should be instituted immediately.

- 1. Repair the upstream paving.
- 2. Monitor the seepage exiting the rock toe at periodic intervals and during periods of high reservoir levels.
- 3. Institute a formal inspection program to be conducted at regular intervals.
- 4. A warning system should be instituted to warn downstream residents of high spillway discharges or during periods of heavy rainfall or high runoff.



10 R. Jeffrey/Kimball



L. ROBERT KIMBALL & ASSOCIATES CONSULTING ENGINEERS AND ARCHITECTS

R. Jeffrey Kimball, P.E.

Date

DACW31-79-C-\$\$\$99

APPROVED BY: (15

16 August 1979

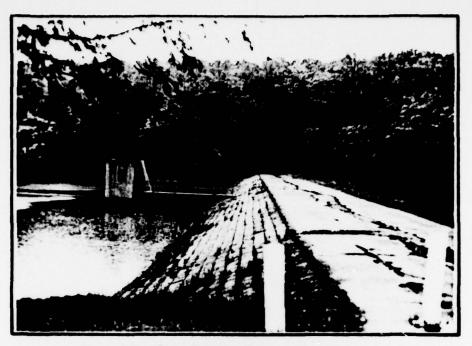
Colonel, Corps of Engineers

District Engineer

6 National Dam Inspection Program. Hunters Lake Dam (NDS ID Number PA-356 DERID Number 57-1) Pennsylvania Fish Commission Susquehanna River Basin, Trout Run, Sullivan Court, Pennsylvania. Phase I Inspection Report,

Aug 79

411059 DW



Overview of upstream slope and crest.



Downstream overview.

TABLE OF CONTENTS

	PAGE
SECTION 1 - PROJECT INFORMATION	1
1.1 General 1.2 Description of Project 1.3 Pertinent Data	1 1 2
SECTION 2 - ENGINEERING DATA	4
2.1 Design 2.2 Construction 2.3 Operation 2.4 Evaluation	4 4 4 4
SECTION 3 - VISUAL INSPECTION	5
3.1 Findings 3.2 Evaluation	. 5 . 6
SECTION 4 - OPERATIONAL PROCEDURES	7
4.1 Procedures 4.2 Maintenance of the Dam 4.3 Maintenance of Operating Facilities 4.4 Warning System in Effect 4.5 Evaluation	7 7 7 7 7
SECTION 5 - HYDRAULICS AND HYDROLOGY	8
5.1 Evaluation of Features5.2 Evaluation Assumptions5.3 Summary of Overtopping Analysis	8 8
SECTION 6 - STRUCTURAL STABILITY	10
6.1 Evaluation of Structural Stability	10
SECTION 7 - ASSESSMENT AND RECOMMENDATIONS/ REMEDIAL MEASURES	11
7.1 Dam Assessment 7.2 Recommendations/Remedial Measures	11 11

APPENDICES

APPENDIX A - CHECKLIST, VISUAL INSPECTION, PHASE I
APPENDIX B - CHECKLIST, ENGINEERING DATA, DESIGN, CONSTRUCTION
OPERATION, PHASE I

APPENDIX C - PHOTOGRAPHS

APPENDIX D - HYDROLOGY AND HYDRAULICS

APPENDIX E - DRAWINGS APPENDIX F - GEOLOGY

PHASE I NATIONAL DAM INSPECTION PROGRAM HUNTERS LAKE DAM NDI I.D. NO. PA 356 DER I.D. NO. 57-1

SECTION 1 PROJECT INFORMATION

1.1 General.

- a. <u>Authority</u>. The National Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.
- b. <u>Purpose</u>. The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 Description of Project.

- a. Dam and Appurtenances. Hunters Lake Dam is an earthfill dam 450 feet long and 27 feet high. The upstream slope is 3H:1V with concrete paving blocks acting as slope protection. The upstream slope in the lower portion is 3.5H:1V. The downstream slope is 2.5H:1V and grassed. The embankment is homogeneous with a rock toe. Upstream of the dam is a concrete control tower which contains the principal spillway. Flow enters the concrete spillway tower and drops down the tower and into a 48 inch reinforced concrete pipe to an impact basin at the toe of the dam. In addition, the concrete spillway tower has a 4 foot by 5 foot sluice gate to act as a reservoir drain. The emergency spillway is located in a natural saddle at the opposite end of the reservoir. The emergency spillway has a 300 foot long concrete slab.
- b. <u>Location</u>. The dam is located on Trout Run, approximately 2.5 miles northwest of Muncie Valley, Sullivan County, Pennsylvania. Hunters Lake Dam can be located on the Eagles Mere, Pennsylvania U.S.G.S. 7.5 minute quadrangle.
- c. <u>Size Classification</u>. Hunters Lake Dam is an intermediate size structure (27 feet high, 2259 acre-feet).
- d. <u>Hazard Classification</u>. Hunters Lake Dam is a high hazard dam. Downstream conditions indicate that loss of more than a few lives is probable should the structure fail. (See section 3.1e).
- e. Ownership. Hunters Lake Dam is owned by the Commonwealth of Pennsylvania, Pennsylvania Fish Commission. Correspondence should be addressed to:

Commonwealth of Pennsylvania Pennsylvania Fish Commission Bureau of Fisheries and Engineering Robinson Lane Bellefonte, Pennsylvania 16823 814-359-2754

- f. Purpose of Dam. Hunters Lake Dam is used for recreation.
- g. <u>Design and Construction History</u>. The dam was constructed by the American Asphalt Company in 1970 replacing a previous dam at the site.
- h. Normal Operating Procedures. The reservoir is maintained at the principal spillway crest with the excess inflow discharging over the principal spillway. During high flows, water flows out the emergency spillway located at the opposite end of the reservoir. Each year the reservoir drain is opened for inspection and lubrication.

1.3 Pertinent Data.

a. Drainage Area.

1.3 square miles

b. Discharge at Dam Site (cfs).

Maximum known flood at dam site	Unknown
Principal spillway capacity at top	
of dam elevation	280
48" drainline at normal pool	Unknown
Emergency spillway capacity at top	
of dam elevation	7560
Total spillway capacity at top of	
of dam elevation	7840

c. Elevation (U.S.G.S. Datum) (feet). - Elevations based on normal pool elevation 1563 shown on U.S.G.S. quadrangle. Elevations shown on construction drawings are from an arbitrary datum.

Top of dam - low point	1568.2
Design top of dam	1568.0
Maximum pool - design surcharge	Unknown
Full flood control pool	N/A
Normal pool	1563.0
Principal spillway crest	1563.0
Emergency spillway crest	1563.8
Upstream portal - 48" drainline	1547.0
Downstream portal - 48" drainline	1541.1
Streambed at centerline of dam	1541.0
Maximum tailwater	None
Toe of dam	1541.1

d. Reservoir (feet).

Length	of	maximum pool	5500
Length	of	normal pool	5500

e. Storage (acre-feet).

Normal pool	1224
Flood control pool	N/A
Design surcharge	Unknown
Top of dam	1840

f. Reservoir Surface (acres).

Top of dam	140
Maximum pool (PMF)	135
Flood control pool	N/A
Normal pool	117
Emergency spillway crest	117

g. Dam.

Type	Earthfill
Length	450 feet
Height	27 feet
Top width	15 feet
Side slopes - Upstream - Upper portion	3H:1V
Lower portion	3.5H:1V
Downstream	2.5H:1V
Zoning	None
Impervious core	None
Cutoff	None
Grout curtain	None

h. Reservoir Drain.

Туре	48" concrete pipe
Length	140 feet
Closure	Sluice gate in concrete tower
Access	Concrete tower
Regulating facilities	Sluice gate in concrete tower

i. Emergency spillway.

Type	Uncontrolled concrete weir
Length	300 feet
Crest elevation	1563.8
Gates	None
Upstream channel	Lake
Downstream channel	Natural drainage

SECTION 2 ENGINEERING DATA

- 2.1 <u>Design</u>. Review of information in the files of the Commonwealth of Pennsylvania, Department of Environmental Resources and the Pennsylvania Fish Commission revealed that construction drawings, design reports, permits and specifications were available. All this data was reviewed for this study.
- 2.2 Construction. The only information available on the construction of the dam were the construction photographs.
- 2.3 Operation. No formal operating records are maintained on water levels and discharges. The operation and maintenance manual for Hunters Lake Dam was reviewed for this study.

2.4 Evaluation.

- a. Availability. Engineering data were provided by PennDER Bureau of Dam Safety, Obstructions and Storm Water Management and by the Pennsylvania Fish Commission. Members of the Pennsylvania Fish Commission staff accompanied the inspection team to answer questions on the construction and operation of the dam.
- b. Adequacy. The type and amount of design data and other engineering information is substantial. The information is sufficient to complete a Phase I Report.

SECTION 3 VISUAL INSPECTION

3.1 Findings.

- a. <u>General</u>. The onsite inspection of Hunters Lake Dam was conducted by personnel of L. Robert Kimball and Associates accompanied by members of the Fish Commission staff on May 24, 1979. The inspection consisted of:
 - 1. Visual inspection of the retaining structure, abutments and toe.
 - Examination of the spillway facilities, exposed portions of any outlet works and other appurtenant works.
 - 3. Observations affecting the runoff potential of the drainage basin.
 - 4. Evaluation of the downstream area hazard potential.
- b. Dam. The dam appears to be in good condition. The dam appears to conform closely to the construction drawings with the exception that an arbitrary datum was used for elevations. From a brief survey conducted during the inspection it was noted that the crest of the dam is fairly even. The low point on the dam was located at the right abutment. The crest is approximately 12 feet wide with a bituminous paving surface. The upstream slope above the water level was measured at 3H:1V and was covered with concrete paving blocks for slope protection. These concrete paving blocks have been displaced at several areas particularly near the water level. The downstream slope is measured at 2.5H:1V and covered with grass. The rock toe is exposed at the downstream toe of the embankment. Seepage was noted exiting from the rock toe and from a CMP pipe located near the toe adjacent to the concrete impact basin. The design drawings indicate that a partial cutoff was provided for the dam. The dam was founded upon glacial till. Under seepage is probable with these conditions.
- c. Appurtenant Structures. The reservoir level is maintained by the principal spillway located in a concrete intake tower in the reservoir. The reservoir is drained by a sluice gate located in a concrete control tower. Water from the principal spillway or from the drain flow through the 48" reinforced concrete pipe beneath the embankment to a concrete basin at the toe of the dam. The control tower and the impact basin appeared to be in good condition. No deterioration of the concrete was noted. The emergency spillway is located at the opposite end of the reservoir. The emergency spillway has a 300 foot long concrete weir. The concrete appears to be in very good condition. The flow through the emergency spillway is diverted to another drainage area (Rock Run).

- d. Reservoir Area. The watershed is covered with woodland. The reservoir slopes are not considered to be susceptible to massive landslides which would affect the storage volume of the reservoir or overtopping of the dam by displacing water.
- e. <u>Downstream Channel</u>. Trout Run downstream of Hunters Lake Dam is a steep narrow channel. Approximately 14 homes are located in the flood area approximately 2 miles downstream of the dam.
- 3.2 Evaluation. In general, the embankment and appurtenant structures appear to be in very good condition and well maintained. The seepage exiting from the downstream rock toe should be monitored to determine if flow increases or is turbid. Note: Considerable precipitation occurred prior to and during the inspection possibly concealing minimum seeps or wet areas. Dry weather inspections by the owner are encouraged.

SECTION 4 OPERATIONAL PROCEDURES

- 4.1 <u>Procedures</u>. The reservoir is maintained at the principal spillway crest (elevation 1563.0). During periods of high runoff the emergency spillway discharges flow into Rock Run. The reservoir drainline and sluice gate are exercised each year.
- 4.2 <u>Maintenance of the Dam</u>. No planned maintenance schedule is utilized. Maintenance of the dam is performed by the Fish Commission staff. Maintenance of the dam is considered good.
- 4.3 Maintenance of Operating Facilities. The sluice gate in the control tower is exercised and lubricated each year. The new valve stem on the sluice gate was installed in 1979. Maintenance of operating facilities is performed by Fish Commission staff. Maintenance of the operating facilities is considered good.
- 4.4 Warning System in Effect. There is no warning system in effect.
- 4.5 <u>Evaluation</u>. Maintenance of the dam and operating facilities is considered good. There is no warning system in effect to warn downstream residents of large spillway discharges or failure of the dam.

SECTION 5 HYDRAULICS AND HYDROLOGY

5.1 Evaluation of Features.

- a. <u>Design Data</u>. Hydraulic and hydrologic information are contained in the construction drawings. This data consists of principal and emergency spillway rating curves and area capacity curves. No other data was available.
- b. Experience Data. No rainfall, runoff or reservoir level data were available. The spillway reportedly has functioned adequately in the past. Maximum water level in the reservoir is unknown.
- c. <u>Visual Observations</u>. The concrete in the emergency spillway and principal spillway appeared to be in good condition. Normal flow is maintained by the principal spillway located in the concrete control tower. In addition to the principal spillway weir a wet well is located in the control tower with removable stoplogs. The sluice gate is located in the control tower to act as a reservoir drain.

The emergency spilway is located at the opposite end of the reservoir. The emergency spillway crest is approximately .8 feet higher that the principal spillway weir. The emergency spillway is 300 feet long. The spillway has low concrete walls on either side 1.7 feet high. Above the concrete wall flow is confined in the natural saddle.

d. Overtopping Potential. Overtopping potential was investigated through the development of the probable maximum flood (PMF) for the watershed and the subsequent routing of the PMF and fractions of the PMF through the reservoir and spillway.

The Corps of Engineers, Baltimore District, has directed that the HEC-1 Dam Safety Version systemized computer program be utilized. The program was prepared by the Hydrologic Engineering Center (HEC), U.S. Army Corps of Engineers, Davis, California, July, 1978. The major methodologies or key input data for this program are discussed briefly in Appendix D.

5.2 <u>Evaluation Assumptions</u>. To enable us to complete the hydraulic and hydrologic analysis for this structure, it was necessary to assume that flow is maintained through the principal spillway.

5.3 <u>Summary of Overtopping Analysis</u>. Complete summary sheets from the computer output are presented in Appendix D.

Peak inflow 4127 Spillway capacity 7840

a. <u>Spillway Adequacy Rating</u>. The Spillway Design Flood (SDF) for this dam is the PMF. The SDF is based upon the hazard and size classification of the dam. Based on the following definition provided by the Corps of Engineers, this spillway is rated as adequate as a result of our hydrologic analysis.

Adequate - Intermediate size dams in which the spillway and reservoir can safely pass the PMF.

The spillway and reservoir are capable of controlling the PMF without overtopping the embankment.

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability.

- a. <u>Visual Observations</u>. The seepage at the toe of the dam should be monitored at periodic intervals and during high reservoir levels. The remainder of the dam appears to be in good condition. No erosion slumping was noted on the slopes. The upstream concrete paving blocks have been displaced particularly at water level. This displacement is believed to be from ice action or erosion under the blocks. Based on the visual observations at the time of inspection, the static stability of the dam appeared to be adequate.
- b. <u>Design and Construction Data</u>. Drill logs and soils testing information were available for review. No stability analysis was performed.
- c. Operating Records. There are no formal operating records for the dam.
- d. <u>Post-Construction Changes</u>. There have been no post-construction changes to the dam.
- e. <u>Seismic Stability</u>. The dam is located in seismic zone l. No seismic stability analysis has been performed. Normally, it can be considered that if a dam in this zone is stable under static loading conditions, it can be assumed safe for any expected earthquake loading. Because of the low risk of seismic occurance and the visual observations, no static analysis is required.

SECTION 7 ASSESSMENT AND RECOMMENDATIONS/REMEDIAL MEASURES

7.1 Dam Assessment.

- a. <u>Safety</u>. The dam appears to be in good condition. The visual observations, review of available information, hydrologic calculations, and past operational performance indicate that Hunters Lake Dam's spillway is adequate. The spillway is capable of controlling the PMF without overtopping. No stability analysis has been performed on the dam. The seepage at the toe of the dam through the rock toe should be monitored at periodic intervals to determine if flow increases or is turbid.
- b. Adequacy of Information. Sufficient information is available to complete a Phase I Report.
- c. <u>Urgency</u>. The recommendations suggested below should be implemented immediately.
- d. <u>Necessity for Further Investigation</u>. No further investigations are required at this time.

7.2 Recommendations/Remedial Measures.

- 1. Repair the upstream paving.
- 2. Monitor the seepage exiting the rock toe at periodic intervals and during periods of high reservoir levels.
- 3. Institute a formal inspection program to be conducted at regular intervals.
- 4. A warning sytem should be instituted to warn downstream residents of high spillway discharges or during periods of heavy rainfall or high runoff.

APPENDIX A

CHECKLIST, VISUAL INSPECTION, PHASE I

CHECK LIST VISUAL INSPECTION PHASE I

NAME	OF D	NAME OF DAM Hunters Lake	rs Lak			COUNTY	Sullivan	STATE PA		ID#	ID# PA 356
TYPE	OF D	TYPE OF DAMEarthfill	thfill.			1		HAZARD CATEGORY	EGORY	High	
DATE(1 (8	NSPECTION	Мау	24.	6261	DATE(s) INSPECTION May 24, 1979 WEATHER	Rainy	TEMPERATURE	2	09	
POOL	ELEV	ATION AT	TIME 0	NI	SPECTION	POOL ELEVATION AT TIME OF INSPECTION 1563.2 M.S.L.	M.S.L. TAILWAT	ER AT TIME	OF INSPECT	NOI.	TAILWATER AT TIME OF INSPECTION None M.S.L.

INSPECTION PERSONNEL:

1mball - L. Robert Kimball and Associates	kensmith - L. Robert Kimball and Associates	Kuang Hwei Chuang - L. Robert Kimball and Associates	- Pennsylvania Fish Commission	- Pennsylvania Fish Commission
R. Jeffrey Kimball - L. Robert K.	James T. Hockensmith - L. Robert	Kuang Hwei Chuang - L. Robert Kir	Jon Grindell - Pennsylvania Fish	Danny Oneill - Pennsylvania Fish

James T. Hockensmith RECORDER

EMBANKMENT

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS	None.	
UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE	None.	
SLOUGHING OR EROSION OF EMBANKMENT AND ABUTMENT SLOPES	None noted.	
VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST	Horizontal alignment appears to be good. Vertical alignment-near right abutment- low point equals 1568.2.	
RIPRAP FAILURES	No riprap. Concrete paving blocks act as slope protection. Displacement and distortment of concrete paving blocks near water level.	level.

EMBANKMENT

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
VEGETATION	Grass on downstream slope.	
JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM	Both abutments appear to be good.	
ANY NOTICEABLE SEEPAGE	Seepage from rock toe. Quantity of seepage undetermined.	
STAFF GAUGE AND RECORDER	None.	
DRAINS	Underdrain in rock toe. Water was flowing out of one of these under drains to left of the impact basin.	

CONCRETE/MASONRY DAMS

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
ANY NOTICEABLE SEEPAGE	N/A	
STRUCTURE TO ABUTMENT/EMBANKMENT JUNCTIONS	N/A	
DRAINS	N/A	
WATER PASSAGES	N/A	
FOUNDATION	N/A	

CONCRETE/MASONRY DAMS

VISUAL EXAMINATION OF SURFACE CRACKS CONCRETE SURPACES	OBSERVATIONS N/A	REMARKS OR RECOMMENDATIONS
STRUCTURAL CRACKING	N/A	
VERTICAL AND HORIZONTAL ALIGNMENT	N/A	
MONOLITH JOINTS	N/A	ix
CONSTRUCTION JOINTS	N/A	
STAFF CAUGE OR RECORDER	N/A	

OUTLET WORKS

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	48" concrete pipe line observed except the discharge concrete appeared to be in good condition.	
INTAKE STRUCTURE	Concrete tower appears to be in good condition.	
OUTLET STRUCTURE	Impact basin appeared to be in good condition.	
OUTLET CHANNEL	Outlet channel was in good condition. No obstructions noted.	
EMERGENCY GATE	Sluice gate on 48" drain line unobserved. The stem was repaired recently.	

UNGATED SPILLWAY

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE WEIR	Good condition.	
APPROACH CHANNEL	Lake.	
DISCHARGE CHANNEL	Discharge channel is a natural drainage way formed by a saddle.	
BRIDGE AND PIERS	None.	

PRINCIPAL SPILLWAY

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE SILL	In good condition.	
INTAKE STRUCTURE	Intake is concrete control tower. It appeared to be in good condition.	
DISCHARGE CHANNEL	48" concrete pipe unobserved.	
BRIDGE AND PIERS	None.	
GATES AND OPERATION EQUIPMENT	None.	

DOWNSTREAM CHANNEL

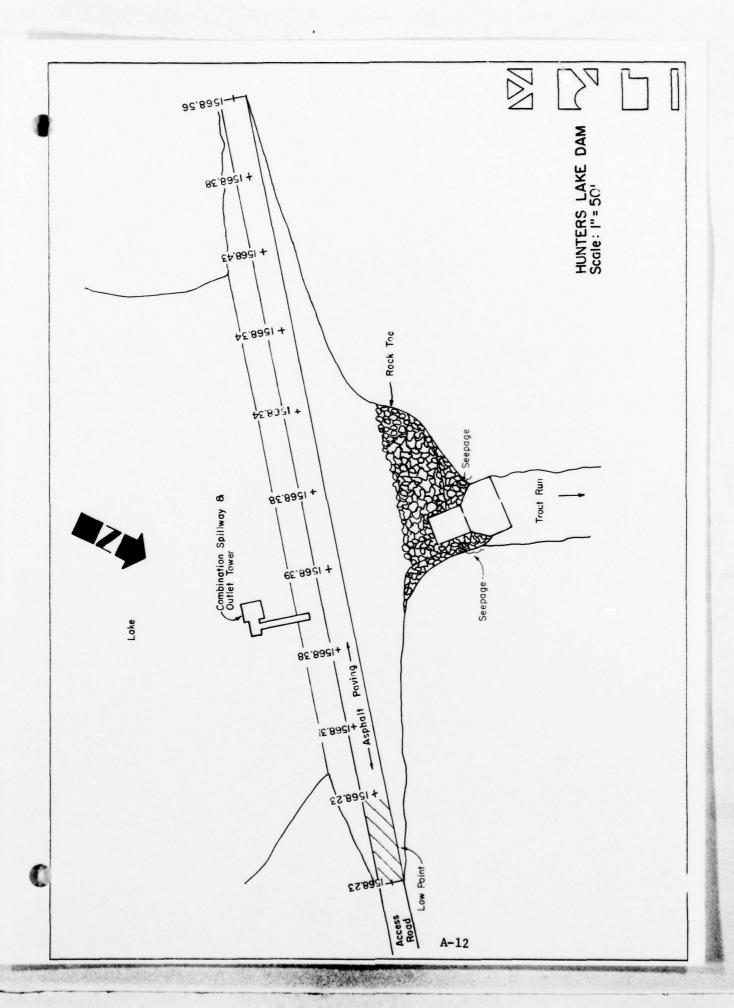
VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)	Narrow and steep downstream channel.	
SLOPES	Slopes appeared to be stable.	
APPROXIMATE NO. OF HOMES AND POPULATION	Approximately 14 homes with 56 people.	

RESERVOIR

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SLOPES	Moderately steep.	
SEDIMENTATION	Minor.	14

INSTRUMENTATION

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
MONUMENTATION/SURVEYS	None.	
OBSERVATION WELLS	None.	
WEIRS	None.	
PIEZOMETERS	None.	•
OTHER	None.	



APPENDIX B

CHECKLIST, ENGINEERING DATA, DESIGN, CONSTRUCTION, OERATION, PHASE I

CHECK LIST
ENGINEERING DATA
DESIGN, CONSTRUCTION, OPERATION
PHASE I

NAME OF DAM Hunters Lake Dam

ID# PA 356

ITEM	REMARKS
AS-BUILT DRAWINGS	None.
REGIONAL VICINITY MAP	U.S.G.S. quadrangle and construction drawings.
CONSTRUCTION HISTORY	Photographs of construction by Pennsylvania Fish Commission.
TYPICAL SECTIONS OF DAM	Construction Drawings.
OUTLETS - PLAN - DETAILS - CONSTRAINTS - DISCHARGE RATINGS RAINFALL/RESERVOIR RECORDS	Construction Drawings.

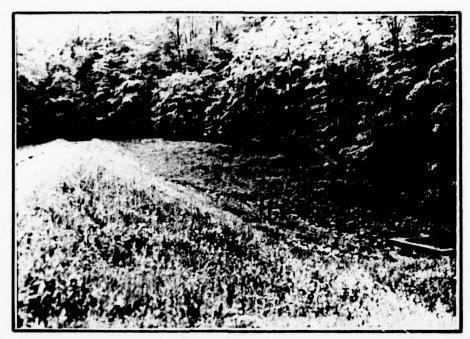
TMON	SARYNAG
DESIGN REPORTS	Report by Geotechnical Services. Report consists of drilling
GEOLOGY REPORTS	and laboratory test results. Geotechnical Services report.
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES	None.
MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY PIELD	Geotechnical Services report.
POST-CONSTRUCTION SURVEYS OF DAM	None.
BORROW SOURCES	Construction drawings.
The state of the s	

ITEM	REMARKS
MONITORING SYSTEMS	None.
MODIFICATIONS	None.
HIGH POOL RECORDS	None.
POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None.
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	Prior to construction of new dam in 1970 the old dam had failed. The old dam was located upstream of the existing dam.
MAINTENANCE OPERATION RECORDS	None.

ITEM	REMARKS
SPILLMAY PLAN SECTIONS DETAILS	Construction drawings.
OPERATING EQUIPMENT PLANS & DETAILS	Construction drawings.

APPENDIX C

PHOTOGRAPHS



Downstream slope and left abutment.



Immediate downstream exposure. Note perforated metal underdrain pipe.



Principal spillway intake.



Inside principal spillway intake.



Spillway weir.



Residence downstream of dam.

APPENDIX D
HYDROLOGY AND HYDRAULICS

APPENDIX D HYDROLOGY AND HYDRAULICS

Methodology. The dam overtopping and breach analyses were accomplished using the systemized computer program HEC-1 (Dam Safety Investigation), September, 1978, prepared by the Hydrologic Engineering Center, U.S. Army Corps of Engineers, Davis, California. A brief description of the methodology used in the analysis is presented below.

1. Precipitation. The Probable Maximum Precipitation (PMP) is derived and determined from regional charts prepared from past rainfall records including "Hydrometeorological Reports No. 40 prepared by the National Weather Service.

The index rainfall is reduced from 10% to 20% depending on watershed size by utilization of what is termed the HOP Brook adjustment factor. Distribution of the total rainfall is made by the computer program using distribution methods developed by the Corps.

2. <u>Inflow Hydrograph</u>. The hydrologic analysis used in development of the overtopping potential is based on applying a hypothetical storm to a unit hydrograph to obtain the inflow hydrograph for reservoir routing.

The unit hydrograph is developed using the Snyder method. This method requires calculation of several key parameters. The following list gives these parameters their definition and how they were obtained for these analysis.

Parameter	Definition	Where Obtained
C _t	Coefficient representing variations of watershed slope and storage	From Corps of Engineers*
L	Length of main stream channel miles	From U.S.G.S. 7.5 minute topographic
L _{ca}	Length on main stream to centroid of watershed	From U.S.G.S. 7.5 minute topographic
C _p	Peaking coefficient	From Corps of Engineers*
A	Watershed size	From U.S.G.S. 7.5 minute topographic

*Developed by the Corps of Engineers on a regional basis for Pennsylvania.

3. Routing. Reservoir routing is accomplished by using Modified Plus routing techniques where the flood hydrograph is routed through reservoir storage. Hydraulic capacities of the outlet works, spillways and the crest of the dam are used as outlet controls in the routing.

The hydraulic capacity of the outlet works can either be calculated and input or sufficient dimensions input and the program will calculate an elevation discharge relationship.

Storage in the pool area is defined by an area - elevation relationship from which the computer calculates storage. Surface areas are either planimetered from available mapping or U.S.G.S. 7.5 minute series topographic maps or taken from reasonably accurate design data.

- 4. <u>Dam Overtopping</u>. Using given percentages of the PMF the computer program will calculate the percentage of the PMF which can be controlled by the reservoir and spillway without the dam overtopping.
- 5. Dam Breach and Downstream Routing. The computer program is equipped to determine the increase in downstream flooding due to failure of the dam caused by overtopping. This is accomplished by routing both the pre failure peak flow and the peak flow through the breach (calculated by the computer with given input assumptions) at a given point in time and determining the water depth in the downstream channel. Channel cross-sections taken from U.S.G.S. 7.5 minute topographic maps were used in the downstream flood wave routing. Pre and post failure water depths are calculated at locations where cross-sections are input.

L. ROBERT KIMBALL & ASSOCIATES
CONSULTING ENGINEERS & ARCHITECTS
EBENSBURG
PENNSYLVANIA

I.D. NUMBER PA. 57-1

SHEET NO. OF 3

BY OTM DATE 6-26-79

HUNTERS LAKE

DRAINAGE AREA

AREA = 1.3 MIZ (FROM U.S.G.S. 7.5-MIN. QUAD.)

UNIT HYDROGRAPH PARAMETERS

DAMBITE LOCATED IN ZONE * 17, SUSQUEHANNA RIVER BASIN. FROM CORPS OF ENGINEERS, BALTIMORE DISTRICT REGIONAL STUDY.

Cp = 0.45 , Ct = 1.13

L= 1.0 mi , La= 0.5 mi (FROM 45.G.S. 7.5-MIN. QUAD.)

tp= (LxLcw) 0.3 = 1.13 (1x0.5)0.3

tp = 0.92 HRS. (SNYDERS LKG (tp) IN HRS.)

LOSS RATE AND BASE FLOW PARAMETERS

AS RECOMMENDED BY CORPS OF ENGINEERS, BALTIMORE DISTRICT.

STRTL = / INCH

CNSTL = 0.05 IN/HR

STRTQ : 1.50 cfs/Mi2

QRCSN : 0.05 (5% OF PEAK FLOW)

RT10R . 2.00

PROBUBLE MAXIMUM STORM

FROM H.R. NO. 40 P.M.P., INDEX BAINFALL = 22.2 (1.0) = 22.2 N.

R6=117%, R12=127%, R24=136%, R48=143%, R72=145%

L. ROBERT KIMBALL & ASSOCIATES
CONSULTING ENGINEERS & ARCHITECTS
EBENSBURG
PENNSYLVANIA

DAM NAME HUNTERS LAKE

I.D. NUMBER PA 57-1

SHEET NO. 2 OF 3

BY OTM DATE G-ZG-79

ELEVATION - AREA - CAPACITY RELATION SHIPS

FROM U.S.G.S. 7.5-MIN. QUAD. , AND DER FILES.

AT SPILLWAY CREST ELEV. = 1563.0'

AREA = 117 ACRES

INITIAL STORAGE = 1224.5 Ac. FT

AT 1600', AREA = 147 AC. AT 1600', AREA = 223 AC.

FROM CONIC METHOD FOR RESERVOIR VOLUME. FLOOD HYDROGRAPH PACKAGE (HEC-1). DAM SAFETY VERSION (USERS MANUAL).

H= 3 V / A = 3 (1224.5) / 117 = 31.4'
ELEVATION AT CAPACITY EQUALS ZERO;
1563'-31.4' = 1531.6'

ELEY. (FT.)	/531.6	1563.	/580	1600
AREA (NC.)	0	117	147	223

DISCHARGE RATING CURVE

PRINCIPAL SPILLWAY FROM:

Q = CLH " (PRETIAL FLOW)
C = 3.3 , L = 20.8

PROM;

Qz= A = 23h (FULL FLOW THEU +8" PIPE)

INVERT ELEV. = 1541.1'

WHERE ZK = 3.24 (FROM CHOW)

M

L. ROBERT KIMBALL & ASSOCIATES CONSULTING ENGINEERS & ARCHITECTS = EBENSBURG

PENNSYLVANIA

DAM NAME HUNTERS LAKE I.D. NUMBER ___ PA. 57-1

> SHEET NO. 3 OF BY OTM DATE 6 - 26-79

EMERCENCY SPILLWAY

FROM; **Q= B.03C'hy 1/2 (hp-hy) [B+Z(hp-hy)]
WHERE hy= 3(ZZhp+B)-1/6ZZhp2+16ZBhp+9BZ)1/2
1/0Z

c'= 0.95

	SER	VICE SI	PILLWA	4	EMER	GENCY	DISCHARGE
ELEV.	WEIR	FLOW	FULL	FLOW	SPILL	-WAY	TOTAL
(FT.)	hi	Q	hz	Qz	hs	Qs	*Q-
	(FT.)	(cfs)	(FT.)	(cfs)	(FT.)	(c5s)	(655)
1563	0	0					0
1563.2	0.2	6					10
1563.5	0.5	24					25
1563.8	0.8	49					50
1564	1	69			2.0	80	150
1565	2	194			1.2	1211	1400
1565.5			22.4	265	1.7	2080	2270
1566			22.9	268	2.2	3//5	3380
1567			23.9	274	3.2	5660	5930
1568			24.9	280	4.2	88/0	9090
1569			25.9	285	5.2	12550	12840
1570			269	291	6.2	16880	17170
1571			27.9	296	7.2	21800	22100
1572	1000		28.9	301	8.2	27330	27630

* CSS YALUES ROUNDED

THE EMERGENCY SPILLWAY WAS ASSUMED TRAPEZOIDAL FOR DISCHARGE CALCULATIONS.

**Q = FROM; WATER AND WASTEWATER ENGINEERING (11-14) &(11-15) by FAIR, GEYER & OKUN

> LOW DAMS Eg. (7) \$ (8) BY NATIONAL RESOURCES COMMITTEE WASHINGTON, D.C. 1938

CHECK LIST HYDROLOGIC AND HYDRAULIC ENGINEERING DATA

DRAINAGE AREA CHARACTERISTICS: 1.3 square miles (wooded, moderately steep)
ELEVATION TOP NORMAL POOL (STORAGE CAPACITY):1563.0 (1228 acre-feet
ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY): N/A
ELEVATION MAXIMUM DESIGN POOL:
ELEVATION TOP DAM:1568.2
SPILLWAY CREST:
a. Elevation1563.8
a. Elevation 1563.8 b. Type concrete weir c. Width 1 foot d. Length 300 feet
c. Width 1 foot
d. Length 300 feet
e. Location Spillover Opposite end of reservoir
f. Number and Type of Gates None
OUTLET WORKS:
a. Type48" concrete pipe
b. Location Through dam
c. Entrance inverts1547.0
d. Exit inverts 1541.1
c. Entrance inverts1547.0 d. Exit inverts1541.1 e. Emergency draindown facilities Sluice gate
TYDROMETEOROLOGICAL GAUGES:
a. TypeNone
b. Location
c. Records
MAXIMUM NON-DAMAGING DISCHARGE:Unknown

			***			2.0		
							4	
				= =				
				: 2				
	3	010		*				
	1 2 4 1 2 4	511		000				
				1367				
		1		130				
	S T T T T T T T T T T T T T T T T T T T	35	-	: 2				
	OF SECTION		34.					
	EN TAN	12	Avoila	1963.	09			
	BRAUC ROUT		Z.O	5 - 50 -	280			
	31	34	* 10	2				
2=	100 0 100 0 100 0 100 0	100	2007		1961			
2 2 2 B	355		7					
2		5 - S - S - S			**			
2 4 8 A								•
4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6								
2 2 2 2				• • • · · · · ·				
123					72.00			
			D	-7				
		GATE .	العجا		Land		اعتقدا	135

The state of the s		1		No.	2/8/	a	-	L. 5		4.1	(C-2)		10.3		l A		-3.7	
LICAN PROPERTY NAME OF STATE O		*				1				.:		-						
LICAN PROPERTY AND THE PARTY OF			-								* 1				3.3			
LICAN PROPERTY AND THE PARTY OF		.5.					1					•						
LICAN PROPERTY AND THE PARTY OF			. :								- Se							
LICAN PROPERTY AND THE PARTY OF									74		7			4	-			
LICAN PROPERTY AND THE PARTY OF										:		00			•			
LAST MODIFICATION AS PER 19 LAST MODIFICATIO												1						
LAST MODIFICATION AS PER 19 LAST MODIFICATIO	المعواة	1	3 10	-		20				:				<i>;</i>			*	
LAST MODIFICATION AS PER 19 LAST MODIFICATIO				1		2 5	2		**			TAGE						-
LAST MODIFICATION AS PER 19 LAST MODIFICATIO				\$4.00 m				14 - 12				2						-
LAST MODIFICATION AS PER 19 LAST MODIFICATIO						F. S.	2		6 300			N.						
LAST MODIFICATION AS PER 19 LAST MODIFICATIO									17 pt.	:		=						
LAST MODIFICATION AS PER 19 LAST MODIFICATIO		3				ې چ						50		,	534			
LAST MODIFICATION AS PER 19 LAST MODIFICATIO			-			=		EĎ		1		4						
LAST MODIFICATION AS PER 19 LAST MODIFICATIO		:32.3			1	4 00	-	8-				-0						
AMALYSIS OF DAM OVERTOPPING USING TOWN OVERTOPPING USING THE PARTY STATES OF DAM OVERTOPPING THE PARTY STATES OF DAM OVERTOPPING USING THE PARTY STATES OF DAM OVERTOPPING USING THE PARTY STATES OF DAM OVERTOPPING THE PARTY STATES OF DAM OVERTOPPI					8	MET		P. C.				4				•		
AMALYSIS OF DAM OVERTOPPING USING TOWN OVERTOPPING USING THE PARTY STATES OF DAM OVERTOPPING THE PARTY STATES OF DAM OVERTOPPING USING THE PARTY STATES OF DAM OVERTOPPING USING THE PARTY STATES OF DAM OVERTOPPING THE PARTY STATES OF DAM OVERTOPPI		2.14	* .		S	E .		W 0			2							
AMALYSIS OF DAM OVERTOPPING USING TOWN OVERTOPPING USING THE PARTY STATES OF DAM OVERTOPPING THE PARTY STATES OF DAM OVERTOPPING USING THE PARTY STATES OF DAM OVERTOPPING USING THE PARTY STATES OF DAM OVERTOPPING THE PARTY STATES OF DAM OVERTOPPI		7	14.		A PASS	NE ST	ō.	2-			9	APE	Server to the	4				
HIT THE PROPERTY OF THE PARTY O		. 13		.0	ZOZ	ŧ		YSES			3	=	GRA)	4.50		- 65	
Control of the contro					200	08 € <		YY.		1	2	20	DRO		20			
AMALYSIS OF DAY AMALYS			•	4.		3	*	3				Ī	Ξ				1	
AMALYSIS OF DAY AMALYS					2 40	. ≥°		49			8	40			1			
AMALYSIS OF DAY AMALYS		3.4			823	-		15		:	=	1001					-	
AMALY SECTION TO SECTI					W A	2.				:	* 0		7 12				- 15	
AMALY SECTION TO SECTI					5	1 1			2			STAG					1	
TANK WOLLD STATE W		-2			5 5 5	39					. 2	-						
BOIL BOIL BUILD BU		100	79		< 10+-	# E					3							
BOIL BOIL BUILD BU		* ± 5		3.							2				1000			
BOIL BOIL BUILD BU		1	35			AN A :				:							The state of	
			Z:	Secretary Section				**	is they			÷,				•	1	
		1 20	A716				10 11 11 11 11 11 11 11 11 11 11 11 11 1	2 4 2 2 2 2	1	1.			re d					
		1 2 2	1610				34	4	1						*			
D-3		101	001	==			7		" red wine	-								
D-3		183	121	5			S. Carrier		and the	71.							Section Section 1	
p-3		123	3	5	4										75.			
p-3		-								7								
p-3				21.0							0		i j					
D-3 200 D-3 20	-			*	3												*	1
		The same of the sa		20				D-3					+		25 Ch 10 Ch			

			100	0 4103 350	225.	11101	
1		6MX R11MP 000 0.00		III ENG T	5		
Silon Some	R12 R96	TL CNSTL AL	08 - 2 · 00 Re 1 · 00 Rough 1 · 00 26 3	W PERTOD W	n 0 - 0 0	151 00	
28.00 000 000 000 000	R24 R46	RTIDK STRT 1.00 1.0 APH DATA	DATA RT 10 - 05 RT 10 - 10 R	ed Row HR.	1.02	1.02 13.5	
SMAP TRSDA 0.00	RG RIZ DO 127:00 13	ERAIN STRKS 0.00 0.00 UNIT HYDROGRA	RECESSION SO GRESN- R CP AND TP AN RICE DRO WATER	S EMD-OF-PER	25.000	00000	
TAREA	PMS 22 200 1174	DLTKR R110L 0.00 1.00	STREET ST	N EXCS LOSS			
own! Sain!	SPFE 01.00 1 MINOGRAM 18	strkn 0.00		PERT OF RAT	00000	000	
	il al majores	LAOPI		Moral Head	10000	1001	
	Applia	-					
		1	p -9				

-		V.	7.46			4	·×	.	* 4	.					
1	3007							,			A. Tr				
			40					8	5	3					
								1567.00					-	-	
C. C								=							-
2000					-					1-					
			ė					8		3			į.		
			1		. 3	1		966.00							
		- ·				7.		-		•			3.5		
		***				0 2	-						1		
C- 15 276						2		5.50			*				
	3000	-00						156							
A 100 00 00 10 10 10 10 10 10 10 10 10 10	253 223 223	5=2			1		\$ 55	-							
XX 32 6	4 -		- 2					0		2			-		
1000	2				1	O d	- 40 00 00 00 00 00 00 00 00 00 00 00 00 0	900				· .			
			•		7	=		15					25		1
	₹	629				o -	3 ×0		•						
10000	2 2	2-7		9	. 5	. <u>8</u>	, , , , , , , , , , , ,	8		3					
200		7.4. 719		=		3		1564							
	2000	000		2	APE	A A A	- 4400 000	=	×.				1		
				APH	=	ISAM	. ₹.								
22.5		200-0		HYDROGRAPH ROUTING	. 3	ROUTING DATA	- 00	1563.80	1972,00	27630.00					
	350	100		YDR	ECO	I R.O.	. 3	1563	1572	163	233				
200	12 -		. 49		7.00				1. A	~			10.		
					VOI	- 9A	5 50	0	•						
	27.				196		2 2	1563.50	1571.00	22100.00	147.				-
		7-2	- E	-	9	~ 8	S. 20-	15	2	722					
100					HROUGH 181	Š	0 0 N						100		
	CFS CMS INCHES	2.5 2.5			THROU			20	CONTRACT OF THE PARTY OF THE PA	3	=				
		2 × 5				0.058		1563.20	15 70.00	17170.00	· 64.		- N - N - N		
		HOUS			2	8	7.	=	=	=					
2.00			3							*	ő				
			-					1563.00	3	2840400					
200			3		-			156	3	2840					
20.00			4.13		7"						1				
	200								2 3	20					
			-					STAGE		9090,000	BURFACE ANEAS		Si alian		200
							*	-	Š	06		4			194
		_ ,,													
			- 4		-		2								
	174.				110										
					1						100	,			
	E A	214	1.3.74			P-10			10.0 on			-		-	-

The State of the S

ELEWATOR: 1353. 1360. 1360. God Città Con Città Con Città Città Con Città Citt	CAPACITYS	1209.	9440.	1120					
15510				•00•			•		
100-EL COOD ERD PANNED 1156612 3.00 ERD PANNED 1156612 3.00 ERD PANNED 1156612 3.00 ERD PANNED 1160614 1: RATIO I 1160614		TO CHEP	*	X		7387 7387	118		
### PERIOD HYDROGRAPH ORDINATES ### PERIOD HYDROGRAPH ORDINATES #### PERIOD HYDROGRAPH ORDINATES ### PERIOD HYDROGRAPH ### PE			1 1		X X X X X	450¢			
ENG-CA-PERIOD HYDRS INFLOW STORAGE MO.DA HR.MN PERIOD HOURS INFLOW STORAGE 101 102 112 112 112 112 112 112 112 112				2	2	ATTO 1. *	**		
			-	-OF-PERIOD H	YDROGRAPH C	ES		AGE	
				2000	2 2 2	000		900	
	D-11	1.01	1.15	4 1.00 5 1.25 4 1.50		000	209- 156	3.0	
1001 2.50 1001 2.50		000		1108					
1.01 4.00 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0			2.00	2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	:	::6	209. 156	000	
1.01 4.00 14 4.25 14 00 1 1 1.01 4.25 14 00 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		100	3.30 3.30 3.45	3.75			2091 201		
		1000	4.00 4.15 4.30	4.00 7 4.25 8 4.50	:::	•••	209• 156 209• 156 209• 156	3.0	
		1001				3	1602		
									4 3

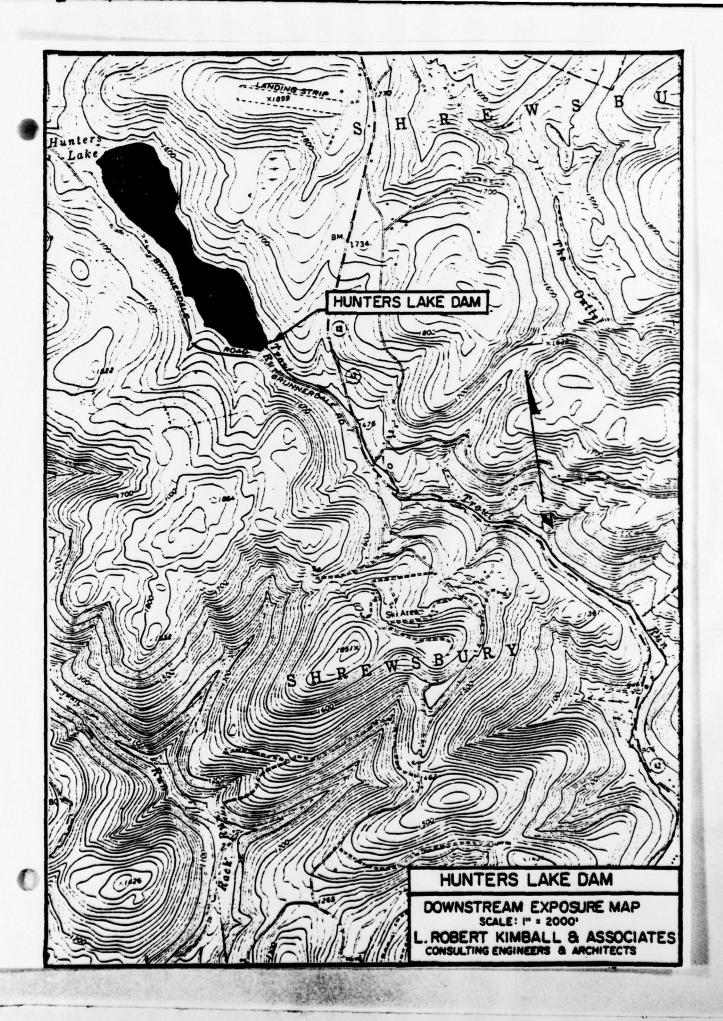
		2.2.4				3	***		
OMS									
I			-					-	**
<u>Cont</u>				5					
- 12 - 12 - 12									
ECONO									
E.	FLOW								
AN-RAT	2								
MULTIPLE PLAN-RAT	RATIOS APPLIED TO			1					
CUBIC	. Y	* 3 -		×					
	14								
ARY FOR	A 1.3								
T III	43 ** 34 74					- 2			
DI SUM FEET P	-0		= Comm					-	
BIC BIC	2:	4127	100.26						
0 N N	¥ Y		9			3 S S S			
TEND	PLAN	****							
IXGE				4					
\$10	AREA	1030	3,371						
. 2								: .	
FLOW AND STORAGE TEL	MOLLAN						10		
PEAK	115					17			
			2.24						
	OPERATION	OGRA/	6						
	OPER	HYDROGRAPH AT ROUTED TO							
		- 4		A 54		N Power S			
		es.			3		13.7		C. 1
Tak te				D-12					*

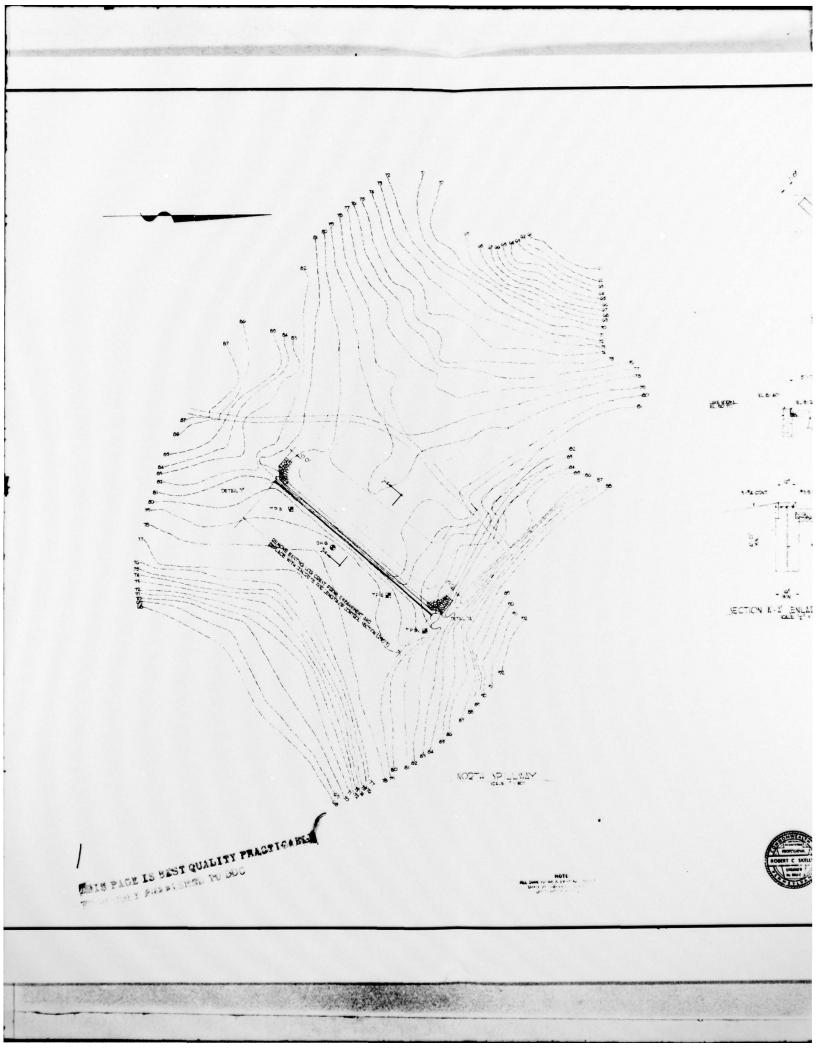
不是想到

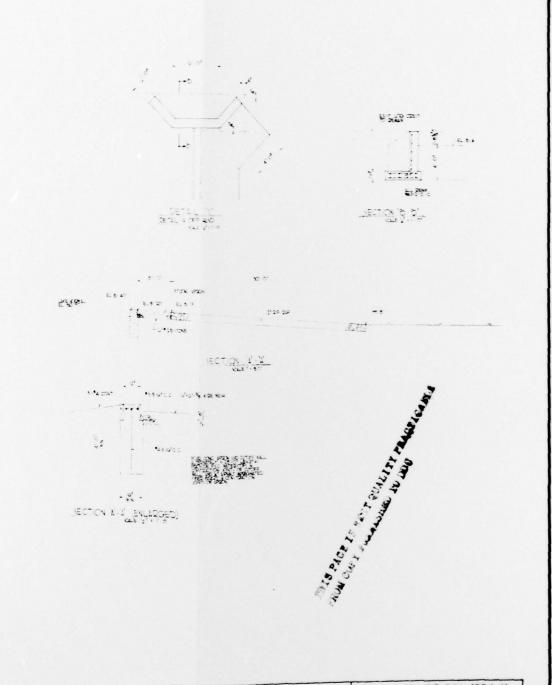
Y CREST YOP OF DAM 1.00 1568.20 209. 1840.	UM DURATION TIME OF TIME OF OW OVER TOP MAX OUTFLOW FAILURE HOURS	90'00 '0'00				
SUMMARY OF DAM SAFETY INTTIAL VALUE SPILLWAY 1563.00 1563	MAXIMUM MAXIMUM MAXIMUM DEPTH \$10RAGE OUTFLOW OVER DAM AC-FT CFS	a heart				
PLÁN 1 ELEVATION STORAGE	161	1566:06				

APPENDIX E

DRAWINGS

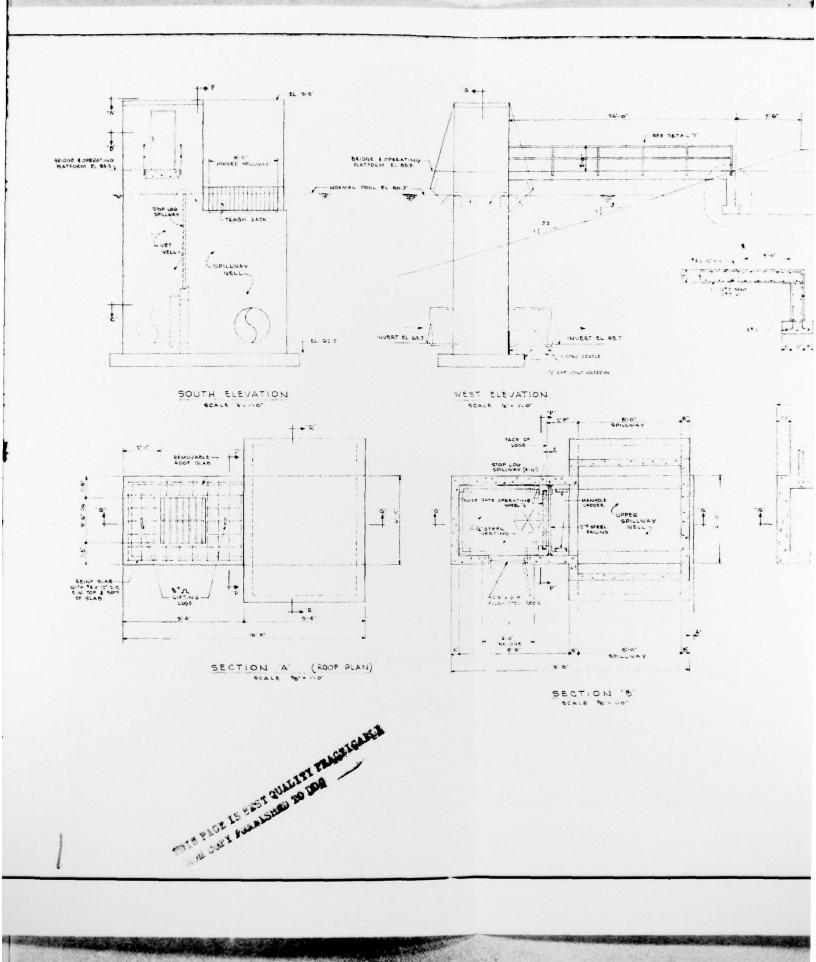


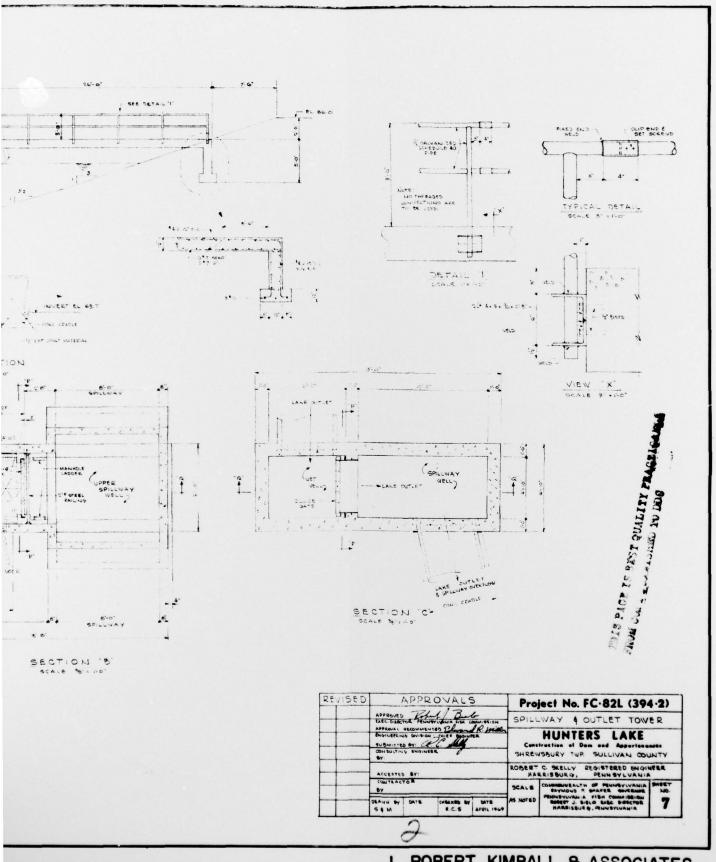


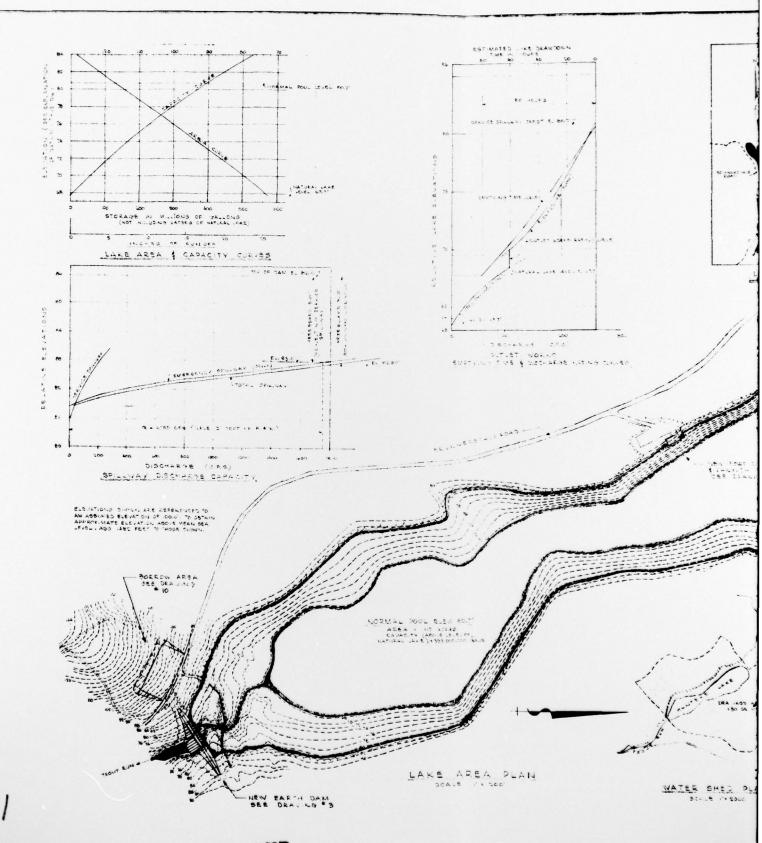


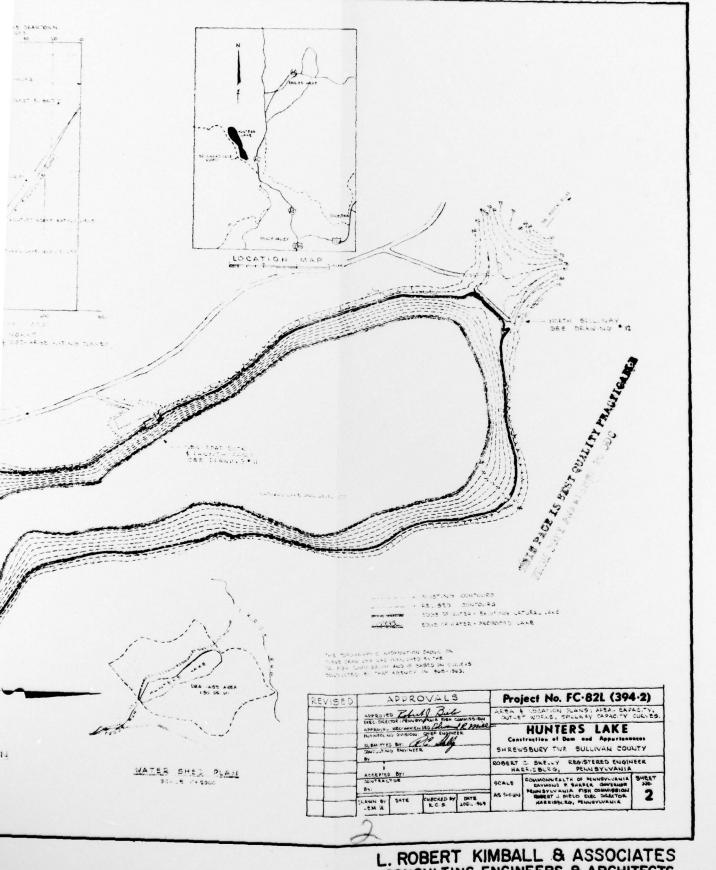


REVISED	APPROVALS	Project No. FC-82L (394-2)					
	SE DELTA PHINSTURA FISH SOMMISS ON	25	CONTRACTOR OF LOT - PLLA	27			
	SEC DESCRIPTION OF THE PROPERTY OF THE PROPERT	SHRE	HUNTERS LAKE	NTY			
-	ACCEPTED BY		COMMONUTATE OF PENSYLVANIA SHEET				
	CONTRACTOR by: DRAWN by DATE CHECKED by DATE 8.0.3 2701 1969	SCALE II WOTED	ENVIOUS I GASEE SANGERER PUNGYUNALLE FISH COMMISSION ROSERT J SELO EXEL DASKTOR WARE SOUR O. PRINTSYLVANIA	12			

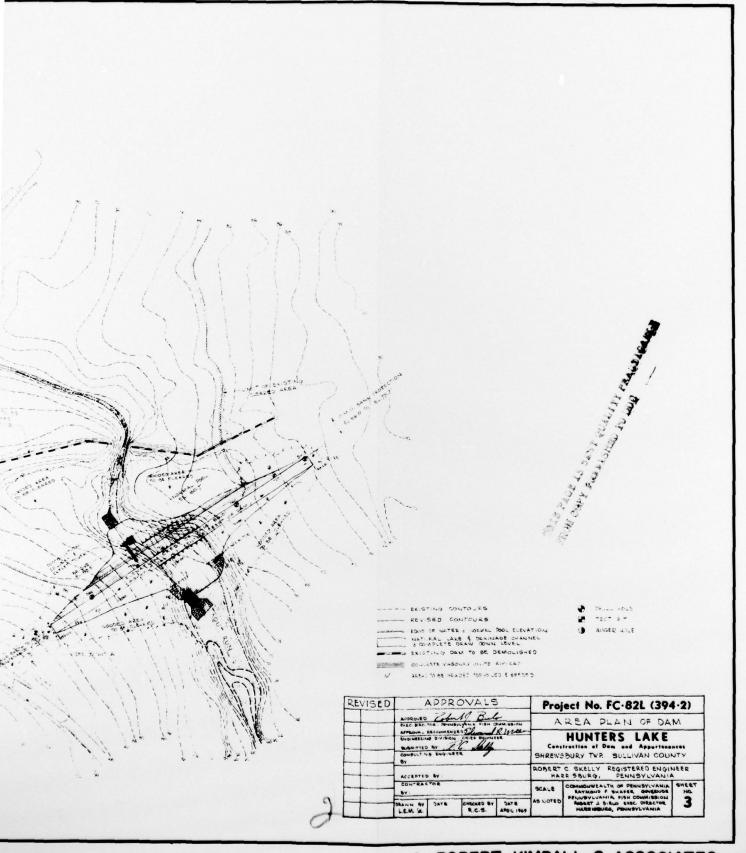


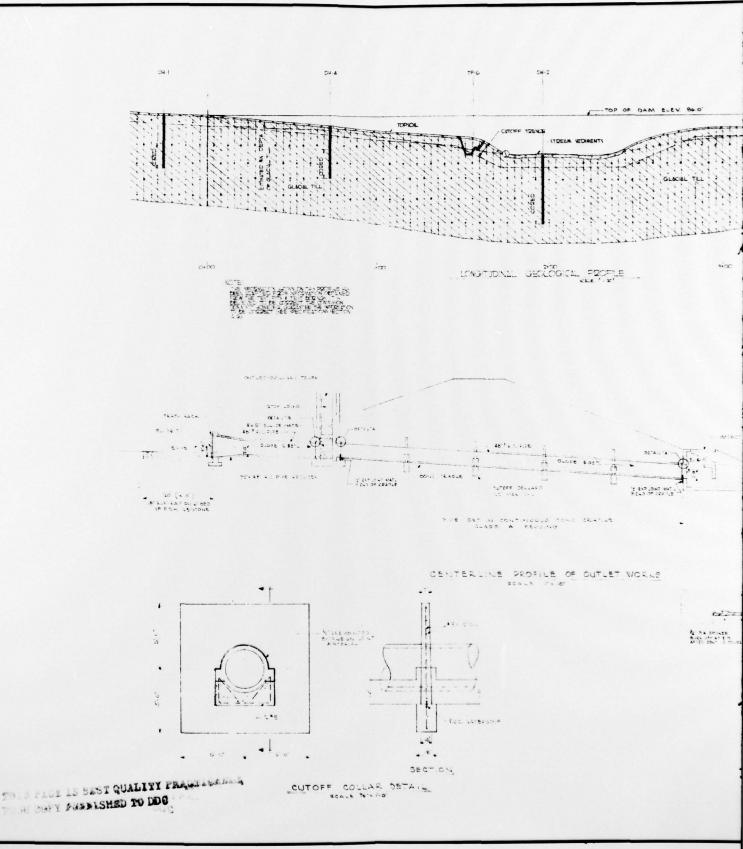


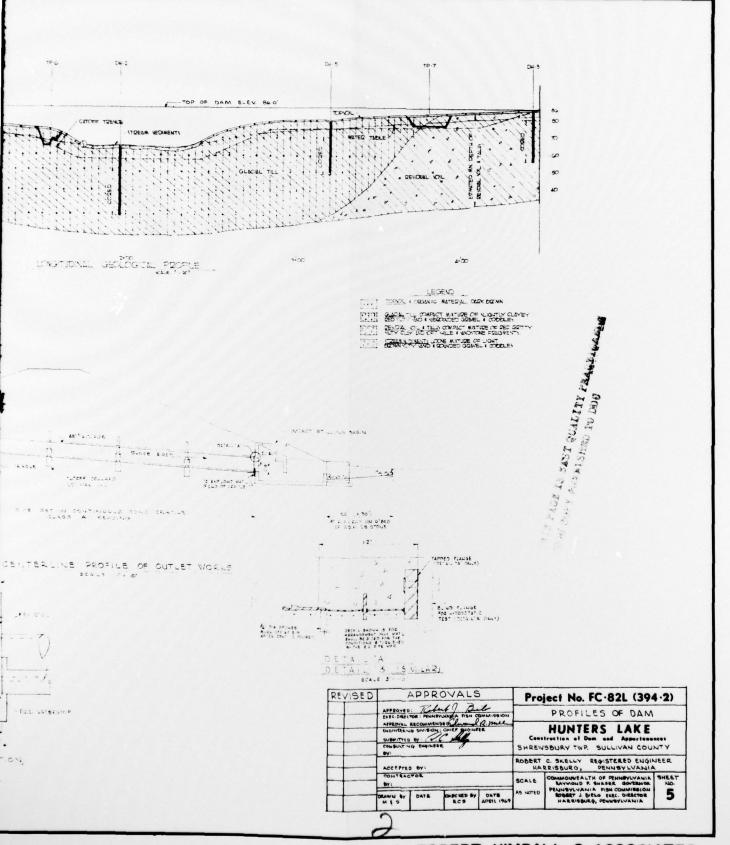












APPENDIX F
GEOLOGY

General Geology.

The Hunters Lake Dam lies within the Glaciated Low Plateaus Section of the Appalachina Plateaus Physiographic Province. This area is characterized by broad anticlines and synclines and little, if any, faulting. The topography has been modified by a blanket of glacial deposits.

The Bedrock under Hunters Lake Dam consists of the Devonian aged Susquehanna Group. This is a complex unit of sandstones, siltstones, shales and conglomerates. Usually the following changes occur from the bottom to the top of the group; the sediment grain size increases, the average thickness of the beds increases, the shales become redder, and the percentage of silica increases. The bedding is usually well developed with thicknesses ranging from less than one to over fifteen feet. The joints are usually closely spaced in a well developed, regular pattern in the shales and siltstones. The shales weather rapidly, while the sandstones, siltstones and conglomerates are moderately resistant. This group can form a good foundation for heavy structures if it is excavated to solid material and the shales and siltstones are kept water free. The surface drainage is moderate to good, except in glaciated regions, such as this one, where it is poor. The interstitial porosity is low in the coarser rocks while the joint development allows a medium quantity of total effective porosity.

The entire area around Hunters Lake has been subjected to depositional affects of continental ice sheets from the Wisconsin Stage of the Pleistocene. Geologic literature indicates that the Wisconsin ice sheet in this area had a thickness of at least 1500 feet and extended as much as five miles of the Sullivan County line. As a result of these glacial features compact preconsolidated deposits of relatively impervious glacial till blanket in the area thickness from a few feet to more than 100 feet. A few isolated deposits of previous outwash sediments from the glacier are scattered throughout the area. The filling and damming of preglacial stream valleys with glacial deposits has resulted in numerous swamps and natural lakes in the area. Hunters Lake on Trout Creek is a natural glacial lake dammed by and resting on a compact, relatively impervious deposit of glacial till. The till is a heterogenious merger of reddish silty and clayey sand with occasionally boulders.



GEOLOGIC MAP OF HUNTERS LAKE AND BEAVER LAKE DAM AREA



Oswayo Formation

OSWAYO FORMATION

Recognish and greenish gray, fine and medium grained sandstones with some shales and scattered categories lines, includes red shales which become more numerous eastward. Relation to type Oswayo not proved.



Catskill Formation

Catskill Formation.
Chefly red to brownish shales and sandstones, includes gray and greenish sandstone longues named Elk Mountain,
Honesiale, Shohola, and Delaware River
in the east.



Marine beds

Gray to olive brown shales, graywackes, and sandstones, contains 'Chemung' beds and 'Portage' beds including Burket, Brallier, Harrell, and Trimmers Rock; Tully Limestone at base.



Scale: 1:250,000

Susquehanna Group

Barbed line is "Chemuno-Catskill" con-tact of Second Pennsylvania Survey County reports; barbs on "Chemung" side of line.